

# HYDRODYNAMICS

TALENT 7:

NUCLEAR THEORY FOR  
ASTROPHYSICS



# FLUID DYNAMICS

Fluid Dynamics, subsuming both hydrodynamics and aerodynamics, is a continuum description of the **collective behavior** of a large number of particles.

The equations of fluid dynamics can be derived from kinetic theory in the limit that the **collisional mean free path**,  $\ell$ , is much smaller than the macroscopic scales of interest,  $L$ .

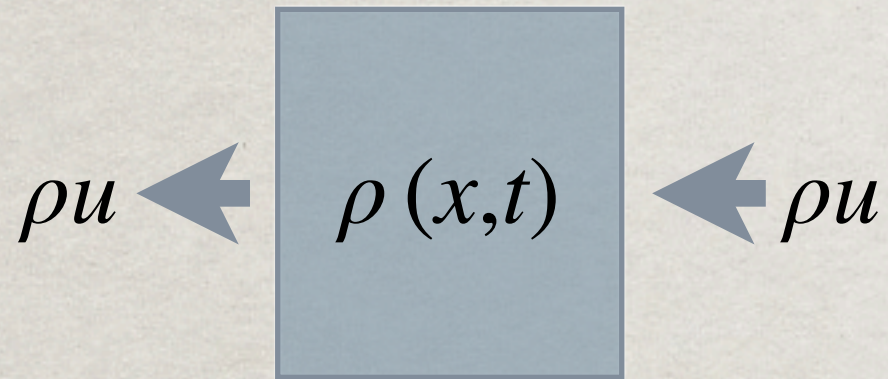
Thus we are concerned with the **bulk velocity** of the fluid,  $u$ , while the random velocity of individual fluid particles is only considered to the extent that they form an **internal energy**.

Key to the behavior of fluids is that they, like solids, deform under stress. However, unlike a solid, a fluid shows no tendency to return to the former state when the stress is removed.



# CONTINUITY

Quantity of matter can be described by the **mass density**, which changes in time and space.



The change of  $\rho$  with time in the box requires a “**flux**” of mass across the boundary at velocity  $u$ .

More formally,

$$\frac{d}{dt} \int_V \rho dV = - \int_S (\rho \vec{u}) \cdot \vec{n} dS$$

Applying the time independence of  $V$  on the left and divergence theorem on the right yields

$$\int_V \frac{\partial \rho}{\partial t} dV = - \int_V \nabla \cdot (\rho \vec{u}) dV$$

Since this is true for arbitrary  $V$ ,

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = 0$$

**Continuity Equation**



# DEFINING DERIVATIVES

When considering a moving fluid, there are two natural frames of reference.

- 1) **Eulerian Coordinates**, which are fixed in space.
- 2) **Lagrangian Coordinates**, which move with the fluid.

To define a **Lagrangian (or material) Derivative** of a quantity  $f$ , we must consider both changes that are **local in space** and those that **result from movement**.

$$\frac{Df}{dt} = \frac{\partial f}{\partial t} + \vec{u} \cdot \nabla f$$

Since  $\nabla \cdot (b\vec{a}) = \vec{a} \cdot \nabla b + b(\nabla \cdot \vec{a})$ , the continuity equation can be transformed from

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = 0 \quad \text{into} \quad \frac{D\rho}{Dt} + \rho \nabla \cdot \vec{u} = 0$$



# CAUSING FLUID TO MOVE

We next need to understand what generates the velocity,  $u$ .

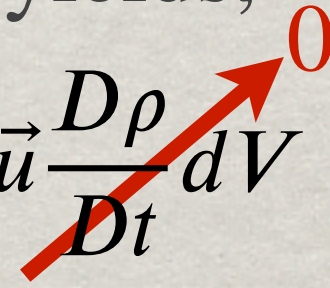
For a co-moving volume, the **total momentum** is  $\int_V \rho u \, dV$  and the time rate of change comes entirely from external forces.

These take the form of external **body forces**,  $f$ , e.g., gravity, and **surface forces**, e.g., pressure,  $P$ .

$$\frac{d}{dt} \int_V \rho \vec{u} \, dV = - \int_S P \vec{n} \, dS + \int_V \rho \vec{f} \, dV$$

Applying the Chain Rule to the left side yields, since  $\rho V$  is invariant for co-moving volumes.

$$\frac{d}{dt} \int_V \rho \vec{u} \, dV = \int_V \rho \frac{D\vec{u}}{Dt} \, dV + \int_V \vec{u} \frac{D\rho}{Dt} \, dV$$



Applying the divergence theorem to the right side yields

$$- \int_S P \vec{n} \, dS + \int_V \rho \vec{f} \, dV = \int_V (-\nabla P + \rho \vec{f}) \, dV$$



# EULER EQUATION

Combining these yields

$$\int_V \rho \frac{D\vec{u}}{Dt} dV = \int_V (-\nabla P + \rho \vec{f}) dV$$

or, since this applies for arbitrary volumes,

$$\rho \frac{D\vec{u}}{Dt} = (-\nabla P + \rho \vec{f})$$

Written in terms of **coordinates fixed in space**, this becomes

$$\rho \left( \frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} \right) = (-\nabla P + \rho \vec{f}) \quad \text{Euler Equation}$$

To make sure we see the physics of this equation, we can rewrite this as

$$\frac{\partial \rho \vec{u}}{\partial t} + \nabla \cdot \rho \vec{u} \vec{u} = -\nabla P + \rho \vec{f}$$



# VISCOSITY

When we wrote the effect of the surface pressure as  $\int_S P \vec{n} dS$ , we implicitly assumed that **viscosity** was unimportant.

In the general case,  $F_i = \int_S \sum_j P \sigma_{ij} n_j dS$ , where  $\sigma_{ij}$  is the **stress tensor**, rather than  $\int_S P n_i dS$ .

For gases and simple liquids, we can define a dynamical viscosity,  $\mu$ , in which case the stress tensor is

$$\sigma_{ij} = -P\delta_{ij} + \mu \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} - \frac{2}{3}(\nabla \cdot \vec{u})\delta_{ij} \right)$$

In this case, the momentum equation becomes **Navier-Stokes**

$$\rho \frac{D\vec{u}}{Dt} = -\nabla P + \rho \vec{f} + \mu \left( \nabla^2 \vec{u} + \frac{1}{3} \nabla(\nabla \cdot \vec{u}) \right) \quad \text{Equation.}$$

$\mu$  is generally very small in astrophysics and the **Reynolds number**, the ratio of inertial forces to viscous forces, is large.



# MECHANICAL ENERGY

The Euler equation includes a gradient of the kinetic energy, requiring an equation to evolve the **kinetic energy**.

Taking the dot product of  $u/\rho$  with the Euler equation

$$\frac{\vec{u}}{\rho} \cdot \rho \frac{D\vec{u}}{Dt} = \frac{\vec{u}}{\rho} \cdot (-\nabla P + \rho \vec{f})$$

provides such an equation

$$\frac{D}{Dt} \left( \frac{1}{2} \vec{u}^2 \right) = -\frac{1}{\rho} \vec{u} \cdot \nabla P + \vec{u} \cdot \vec{f} \quad \text{mechanical energy equation}$$

Simply, the kinetic energy changes in response to **work done by pressure and body forces**.

This approach may seem arbitrary, but is equivalent to calculating the **work done by a force** as

$$uF = uma = um \frac{du}{dt} = \frac{d}{dt} \left( \frac{1}{2} u^2 \right)$$



# ENERGY CONSERVATION

Of course, kinetic energy is not conserved, rather it is the total energy, **kinetic + internal** (thermal),  $\frac{1}{2}u^2 + U$ .

If we expand our energy equation to include the internal energy, we must add terms for the **heat generated** within the volume,  $\epsilon$ , and the **flux of heat** across the boundary,  $F$ .

$$\begin{aligned} \frac{d}{dt} \int_V \left( \frac{1}{2} \vec{u}^2 + U \right) \rho dV = & - \int_S \vec{u} \cdot P \vec{n} dS + \int_V \vec{u} \cdot \vec{f} \rho dV \\ & + \int_V \epsilon \rho dV - \int_S \vec{F} \cdot \vec{n} dS \end{aligned}$$

Applying the divergence theorem to replace the surface integrals

$$\begin{aligned} \int_S \vec{F} \cdot \vec{n} dS &= \int_V \nabla \cdot \vec{F} dV \\ \int_S \vec{u} \cdot P \vec{n} dS &= \int_V \nabla \cdot P \vec{u} dV \end{aligned}$$



# ENERGY EQUATION

As in the prior derivation, the **invariance of  $\rho V$**  for co-moving volumes simplifies the energy time derivative.

$$\frac{d}{dt} \int_V \left( \frac{1}{2} \vec{u}^2 + U \right) \rho dV = \int_V \rho \frac{D}{Dt} \left( \frac{1}{2} \vec{u}^2 \right) + \int_V \rho \frac{DU}{Dt} dV$$

Once again, we can also remove the volume integral that appears in each term, yielding.

$$\rho \frac{D}{Dt} \left( \frac{1}{2} \vec{u}^2 \right) + \rho \frac{DU}{Dt} = -\nabla \cdot P\vec{u} + \rho\vec{u} \cdot \vec{f} + \rho\epsilon - \nabla \cdot \vec{F}$$

Expanding the **co-moving derivatives**, and merging like terms, leaves

$$\begin{aligned} \frac{\partial}{\partial t} \rho \left( \frac{1}{2} u^2 + U \right) + \nabla \cdot \left( \rho \left( \frac{1}{2} u^2 + U \right) \vec{u} \right) \\ = -\nabla \cdot P\vec{u} + \rho\vec{u} \cdot \vec{f} + \rho\epsilon - \nabla \cdot \vec{F} \end{aligned}$$



# EQUATION OF STATE

The **pressure**,  $P$ , appears in both the momentum and energy equation, yet we have no equation for its evolution.

For all matter, there exist **thermodynamic relations** linking the pressure, density, temperature, internal energy, entropy...

These are the **Equations of State** (EoS).

The most widely known is the ideal (monatomic) gas EoS

$$P V = R T \text{ and } U = \frac{3}{2} R T, \text{ thus } P = \frac{2}{3} \rho U$$

The more generalized version is cast in terms of the **adiabatic index**  $\gamma = C_P/C_V$ , the ratio of specific heats.

$$P = (\gamma - 1) \rho U$$

where  $\gamma = 5/3$  for a monatomic gas.



# POLYTROPIC FLUID

For the adiabatic case, the ideal gas EoS can be written as

$$P = K\rho^\gamma \quad \text{in which case} \quad U = \frac{P}{\gamma - 1} = \frac{K\rho^\gamma}{\gamma - 1}$$

Such EoS are often written in the form

$$P = K\rho^{1+\frac{1}{n}} \quad \text{where } n \text{ is called the polytropic index.}$$

These polytropic EoS played a large role in early calculations of stellar structure and remain useful because a number of physical states behave approximately as polytropes.

For example, both the ideal monatomic gas and a non-relativistic degenerate gas obey  $P = K\rho^{5/3}$ .

For a relativistic degenerate gas  $P = K\rho^{4/3}$ , and stars in radiative equilibrium also follow this relation.



# HYDROSTATIC EQUILIBRIUM

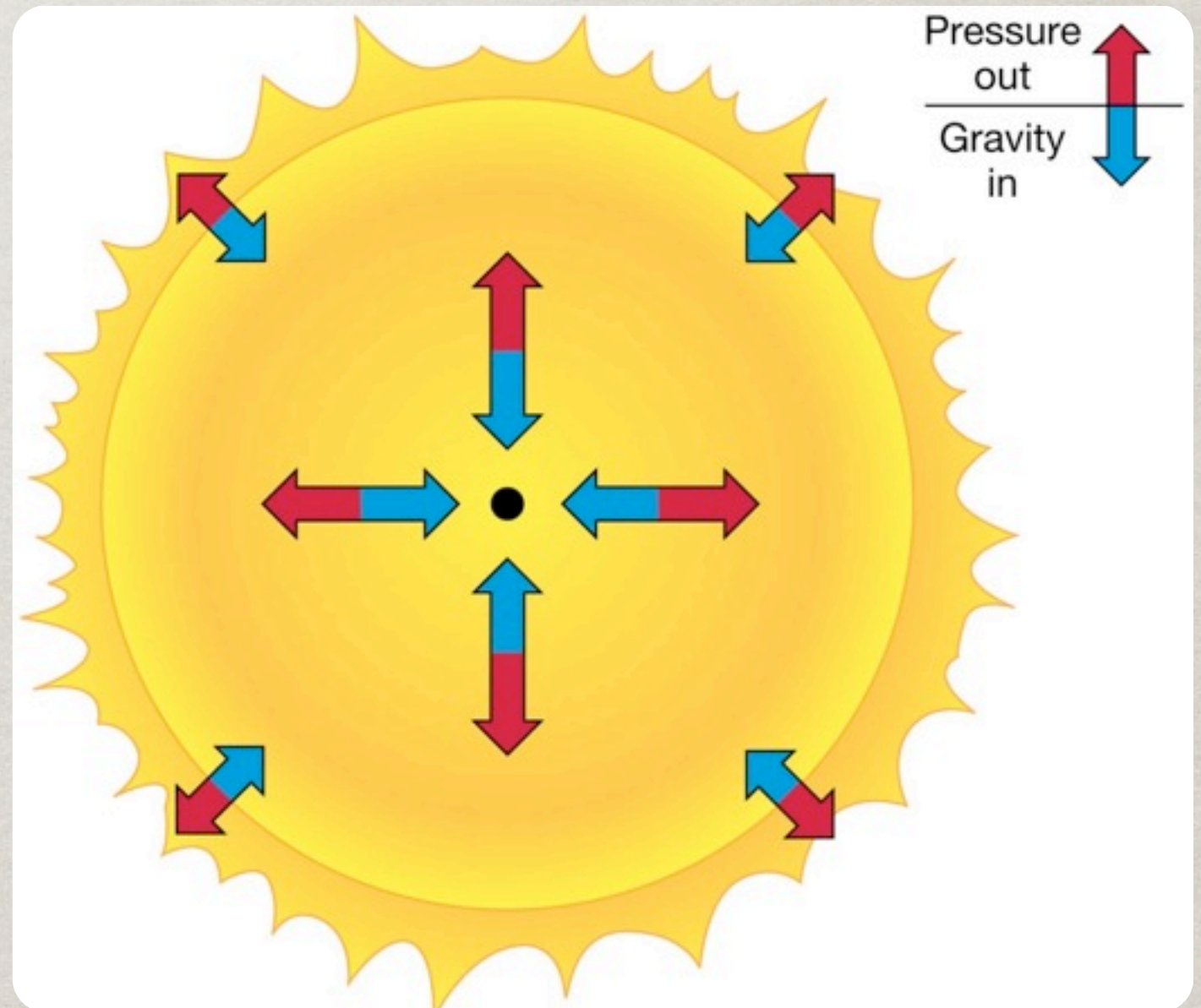
Simplest application of hydrodynamic is hydrostatics ( $u = 0$ ).  
The hydrostatic limit of the Euler equation is *Hydrostatic Equilibrium*.

Numerically this takes the form

$$\frac{dP}{dr} = -\frac{GM(r)\rho(r)}{r^2}$$

Physically, this says the inward gravitational force must be **balanced** by the outward pressure.

This relationship is key to calculating the conditions in a star's **interior**.





# STANDARD SOLAR MODEL

Hydrostatic versions of the continuity and energy equation give us

Mass Continuity

$$\frac{dM}{dr} = 4\pi r^2 \rho(r)$$

Energy Generation

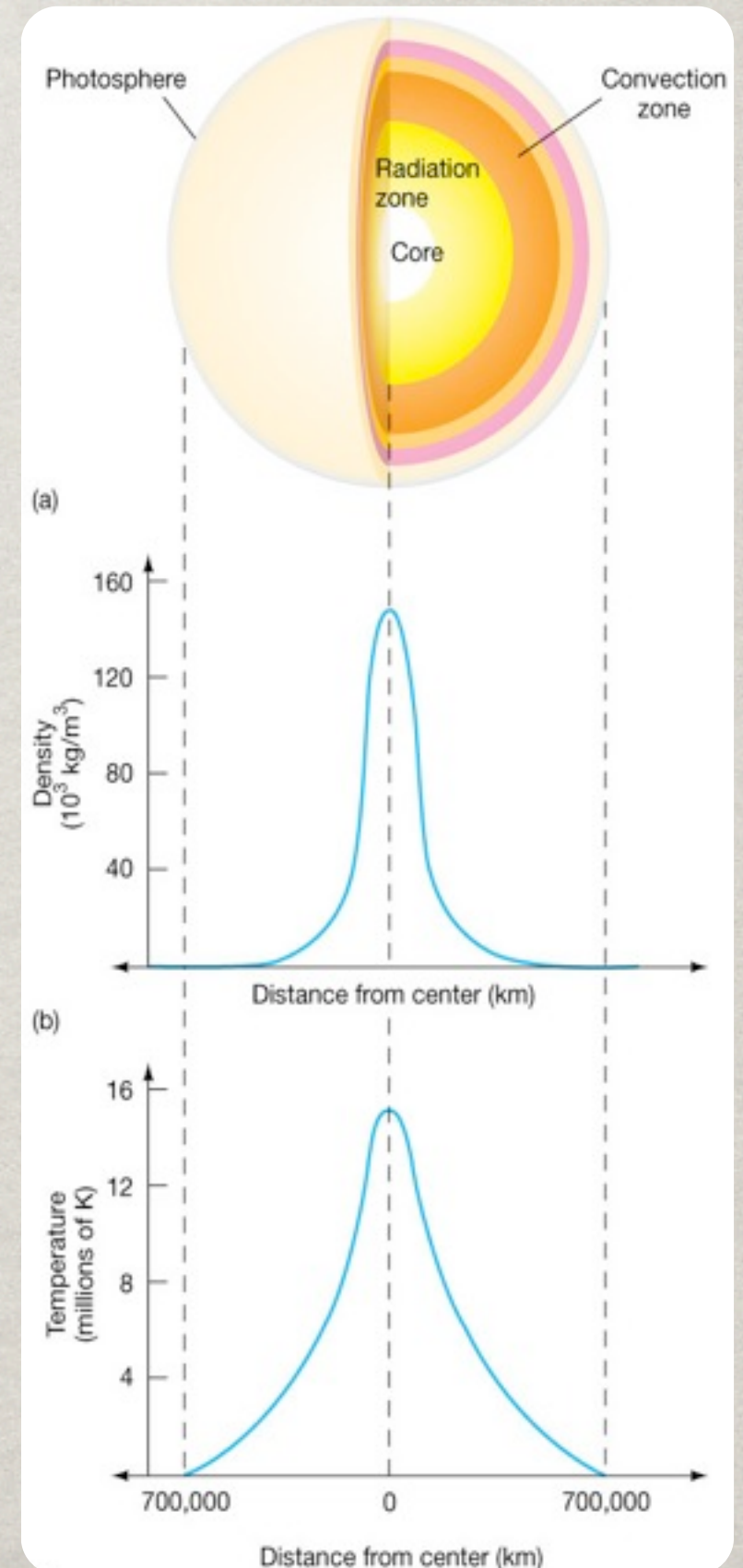
$$\frac{dL}{dr} = 4\pi r^2 \rho(r) \epsilon(r)$$

Together with an equation for **Energy Transport**, which depends on the dominant energy transport process, these combined with boundary conditions like

$$M(0) = 0, L(0) = 0, \&$$

$$M(R_{\odot}) = M_{\odot}, L(R_{\odot}) = L_{\odot}, \text{ etc.}$$

allow us to calculate the **stellar models**.





# THE EQUATIONS WE SOLVE

In VH-1, and many similar hydrodynamics codes, the 3D problem is *directionally-split* into separate 1D solutions along the representative directions. This simplifies the equations.

$$\frac{\partial \rho}{\partial t} + \frac{\partial A \rho u}{\partial V} = 0$$

To allow for **different coordinate systems**, we work in terms of a volume coordinate  $V$  with cell cross section  $A$

$$\frac{\partial \rho u}{\partial t} + \frac{\partial A \rho u^2}{\partial V} = -\frac{\partial P}{\partial \chi} + \rho f$$

Gradients use a generalized spatial coordinate,  $\chi$

$$\frac{\partial \rho v}{\partial t} + \frac{\partial A \rho v u}{\partial V} = 0 = \frac{\partial \rho w}{\partial t} + \frac{\partial A \rho w u}{\partial V}$$

Momentum is also **advected transversely**.

$$\frac{\partial \rho E}{\partial t} + \frac{\partial A \rho E u}{\partial V} = -\frac{\partial A \rho P u}{\partial V} + \rho u f$$

**Total energy  $E = \frac{1}{2}(u^2 + v^2 + w^2) + U$**

$$P = (\gamma - 1)\rho U$$

Equation of State



# SPATIAL DIFFERENCING

Transforming **continuous variables**,  $f(x)$ , to variables represented on a **discrete grid**,  $f_j$ , we must approximate spatial derivatives as **differences**. However, the choice is not unique.

For example,  $\partial f / \partial x$  at  $x = x_j$  can be written as

$$\left. \frac{\partial f}{\partial x} \right|_j \approx \frac{f_{j+1} - f_j}{\Delta x} \quad \text{forward difference}$$

$$\left. \frac{\partial f}{\partial x} \right|_j \approx \frac{f_j - f_{j-1}}{\Delta x} \quad \text{backward difference}$$

$$\left. \frac{\partial f}{\partial x} \right|_j \approx \frac{f_{j+1} - f_{j-1}}{2\Delta x} \quad \text{centered difference}$$

Higher order derivatives **touch more points** on the grid, e.g.,

$$\left. \frac{\partial^2 f}{\partial x^2} \right|_j \approx \frac{f_{j+1} - 2f_j + f_{j-1}}{\Delta x^2}$$



# ORDER OF ERROR

Different choices of derivatives affect **the error that comes from mapping to a discrete grid**. One can estimate this error by calculating  $f_{j+1} = f(x_{j+1}) = f(x_j + \Delta x)$  and  $f_{j-1} = f(x_{j-1}) = f(x_j - \Delta x)$  using the Taylor series

$$f(x + h) = f(x) + h \frac{\partial f}{\partial x} + \frac{h^2}{2} \frac{\partial^2 f}{\partial x^2} + \dots$$

to calculate the error as a function of  $\Delta x$ .

For both forward and backward differencing the leading error in the approximation of  $\partial f / \partial x$  is  $\propto (\Delta x) \partial^2 f / \partial x^2$ , thus these approximations are  **$O(\Delta x)$** . For centered differencing, the error is  **$O(\Delta x^2)$**  because the  $\partial^2 f / \partial x^2$  terms cancel.

While having a smaller **truncation error**, centered differencing has a tendency to spread sharp features which is detrimental in some circumstances.



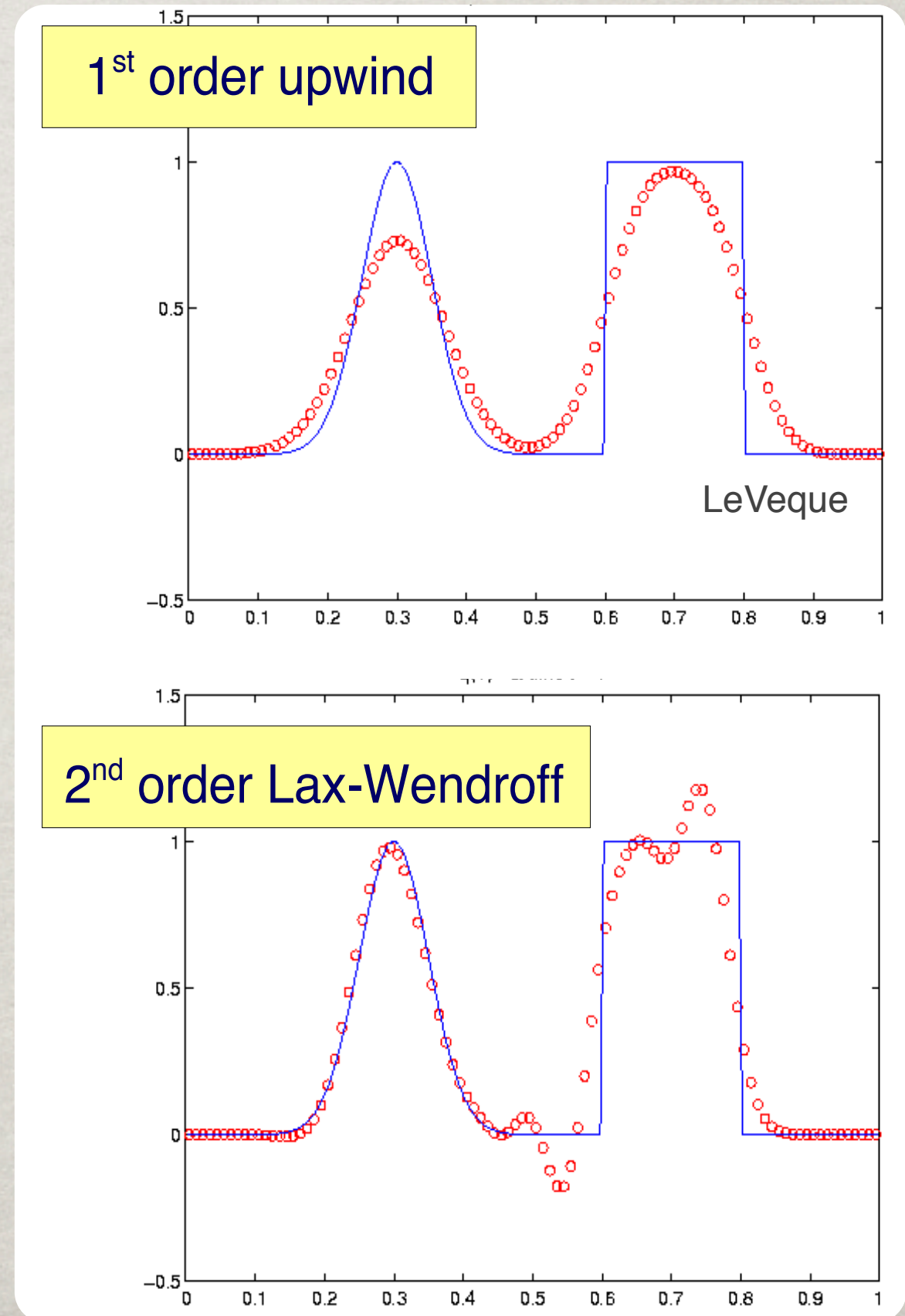
# CAPTURING SHOCKS

Many problems in nuclear astrophysics include shocks and compositional (contact) discontinuities.

Simple differencing schemes are challenged by **sharp flow features** like these.

Low order methods tend to **diffuse** these features over many zones.

Higher order methods are less diffusive, but can add considerable **dispersion** (noise).





# RIEMANN PROBLEM

An alternative, from Godunov, is to calculate fluxes by assuming a **Riemann problem** at each interface.

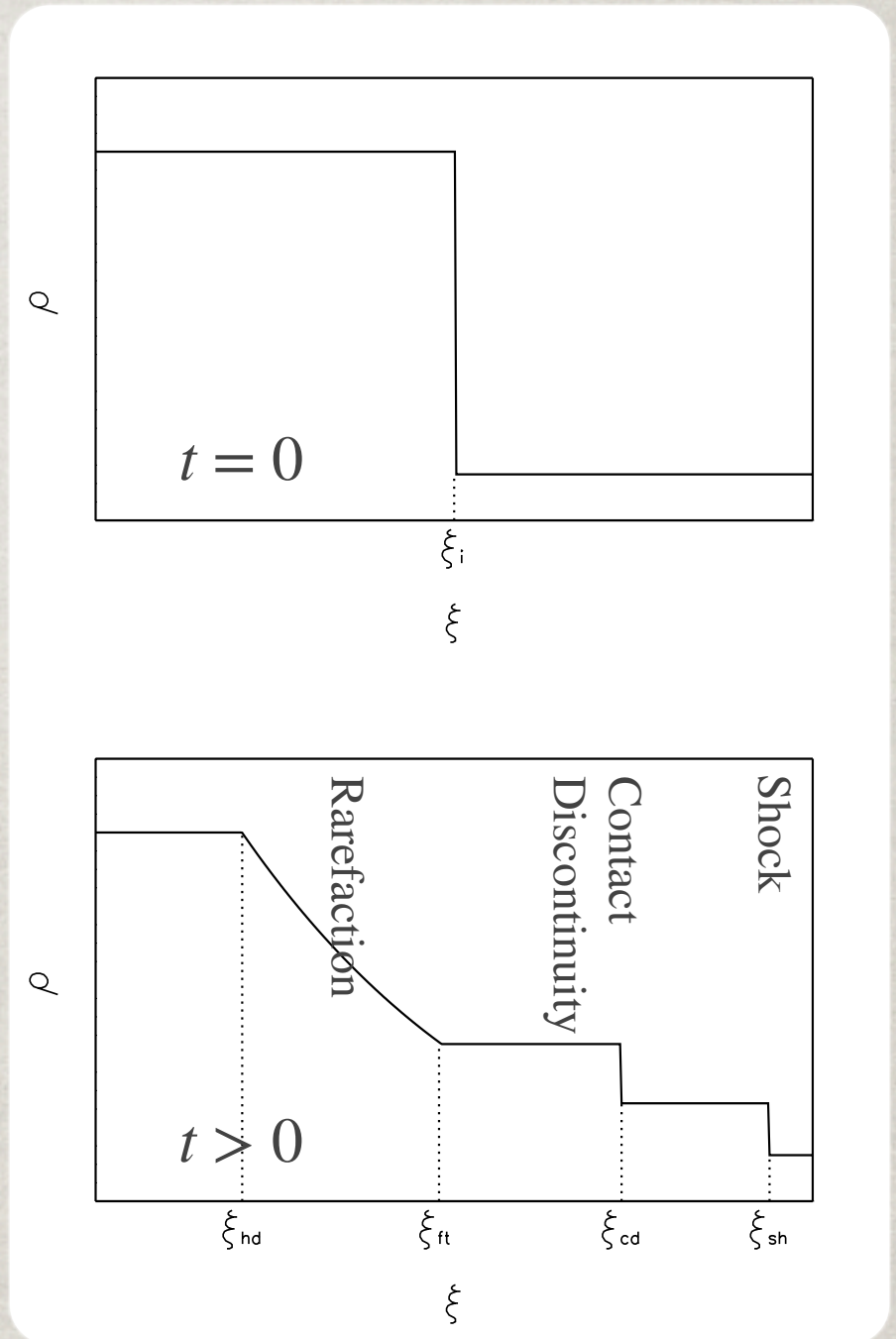
For left wave,  $P^* - P_l + W_l(u^* - u_l) = 0$

For right wave,  $P^* - P_r - W_r(u^* - u_r) = 0$

where  $(P_r, u_r)$  &  $(P_l, u_l)$  characterize the unshocked right and left states,  $(P^*, u^*)$  are the **unknown shocked state** and

$$W_s = \rho_s c_s \left[ 1 + \frac{\gamma + 1}{2\gamma} \left( \frac{P^* - P_s}{P_s} \right) \right]^{1/2}$$

$(P^*, u^*)$  can be calculated (iteratively) from the right and left wave equations and from these **fluxes at the interfaces**.



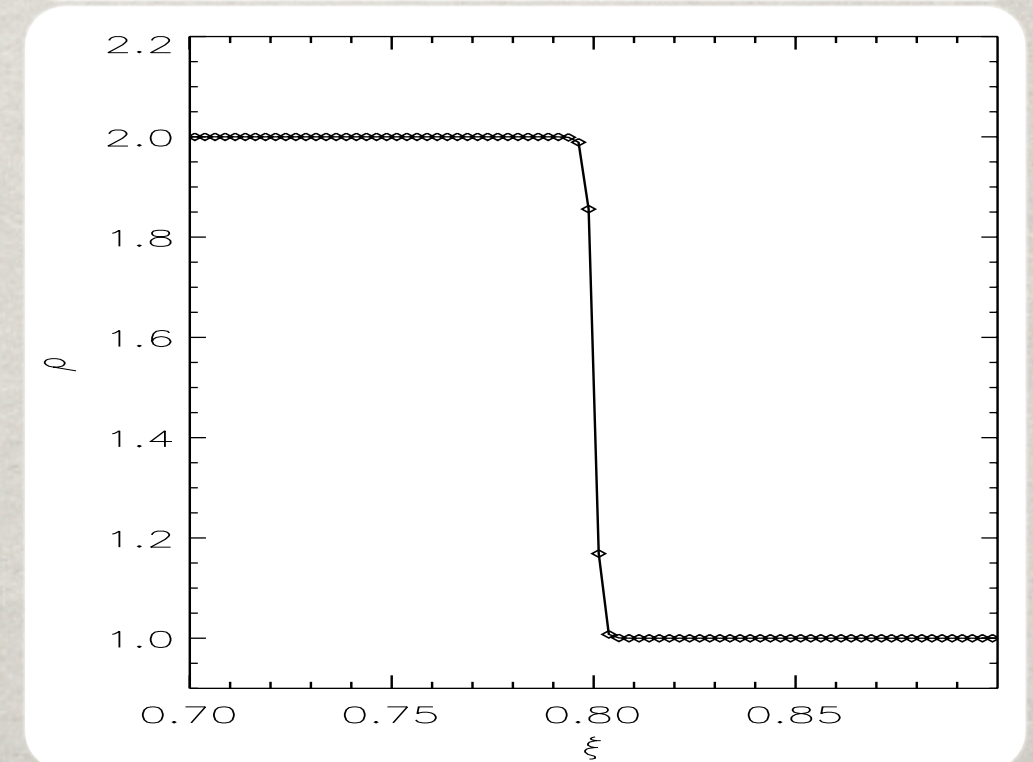
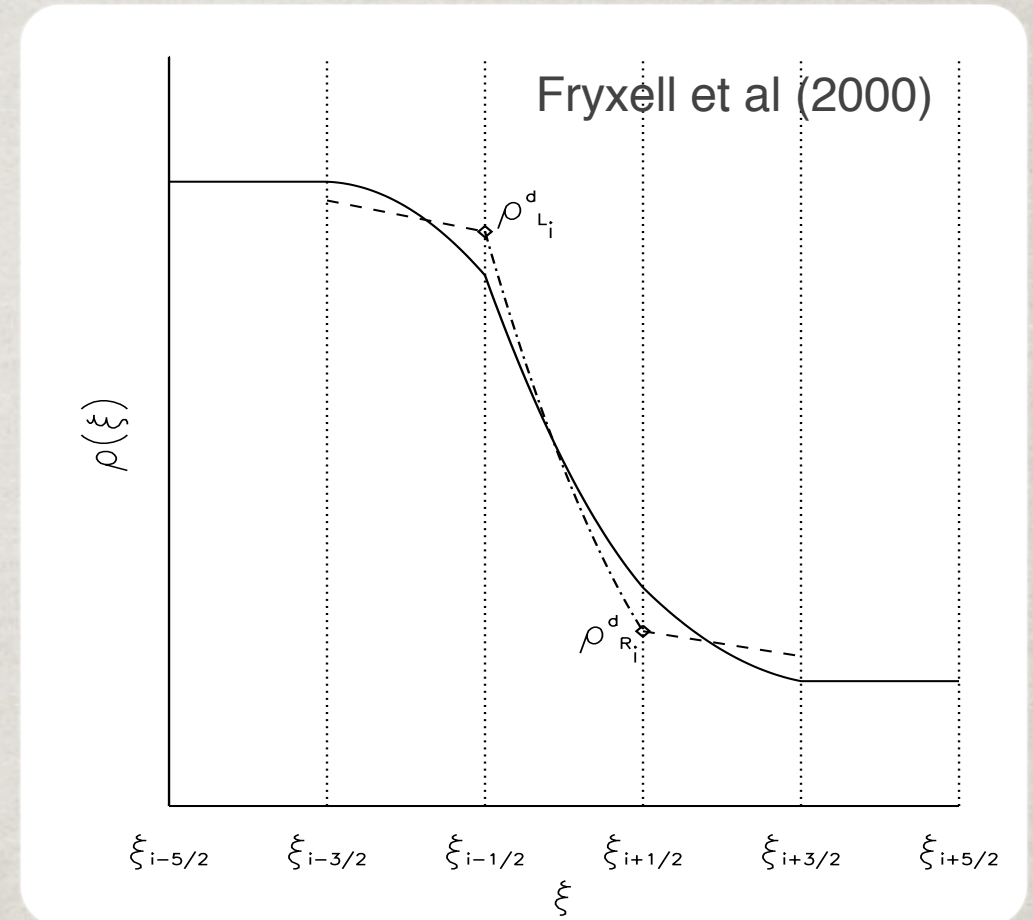


# PPM

The **Piecewise Parabolic Method**, introduced by Colella & Woodward, improves on **Godunov's method** by using a piecewise parabolic reconstruction of flow variables (akin to Simpson's rule for integration) in place of piecewise constant.

It adds explicit steepening of **contact discontinuities** and flattening of overly narrow **shocks**.

FLASH and VH-1 are both implementations of PPM.





# HEAT TRANSPORT

To quantify how the tremendous heat of stellar interior is transferred to the surface, we need an equation for **energy transport**,  $dT/dr = ?$

The form of the equation depends on the means by which the energy moves.

In general, there are **three** modes of heat transfer

**Conduction:** The transfer of energy through motions on the microscopic scale (atoms or molecules).

**Convection:** The transfer of energy through macroscopic fluid motions.

**Radiation:** The transfer of energy via electromagnetic radiation (other forms of radiation are possible).



# RADIATION FORCE

Blackbody radiation exerts a **pressure** equal to  $\frac{1}{3}$  of the radiation density.

$$P_{rad} = \frac{a}{3} T^4 \quad \text{where } a = \frac{4\sigma_{SB}}{c}$$

The **decline in temperature** from the center of the star toward the surface causes a spherical shell in the star, thickness  $dr$ , to experience a **temperature gradient**,  $dT$ .

Inner Surface:

$$P_{rad}(r) = \frac{a}{3} T^4$$

Outer Surface:

$$\begin{aligned} P_{rad}(r + dr) &= \frac{a}{3} (T + dT)^4 \\ &= \frac{a}{3} T^4 \left(1 + \frac{dT}{T}\right)^4 \approx \frac{a}{3} T^4 \left(1 + 4\frac{dT}{T}\right) \end{aligned}$$

This produces a **net force**,

$$\begin{aligned} F_{rad} &= 4\pi r^2 [P_{rad}(r) - P_{rad}(r + dr)] \approx -4\pi r^2 \frac{a}{3} T^4 \frac{4dT}{T} \\ &\approx -\frac{16\pi}{3} r^2 T^3 dT \end{aligned}$$



# RADIATION MOMENTUM

An alternative way to approach the same problem is in terms of the **momentum** of photons that are **absorbed**.

The momentum of a photon is  $p = E/c$ .

The total rate of photon energy passing through the shell is  $L(r)$ , thus the total photon momentum is  $L(r)/c$ .

The **fraction** of the photons **absorbed** passing through a shell of thickness  $dr$  is

$$dI/I = -n(r) \sigma(r) dr = d\tau = -\rho(r) \kappa(r) dr \text{ if } d\tau \ll 1$$

The rate at which **momentum** is **transferred** to the matter by absorbed photons is a force,

$$F_{rad} = \frac{L(r)}{c} \frac{dI}{I} = -\frac{L(r)}{c} \rho(r) \kappa(r) dr$$



# RADIATIVE HEAT TRANSPORT

With 2 equations for  $F_{rad}$ , one in terms of a **temperature change** and the other in terms of a **distance** and opacity, a **temperature gradient** can be constructed.

$$F_{rad} \approx -\frac{16\pi}{3} r^2 T^3 dT = -\frac{L(r)}{c} \rho(r) \kappa(r) dr$$

The resulting gradient,

$$\frac{dT}{dr} = -\frac{3\rho(r)\kappa(r)L(r)}{16\pi ac T(r)^3 r^2} = -\frac{3\rho(r)\kappa(r)L(r)}{64\pi\sigma_{SB} T(r)^3 r^2}$$

is called the *equation of radiative energy transport*.

In the Sun, a typical value of this gradient is

$$\frac{\Delta T}{\Delta r} \approx \frac{T_{surface} - T_c}{R_{\odot} - 0} \approx \frac{5800\text{K} - 1.5 \times 10^7 \text{K}}{7.0 \times 10^5 \text{km}} \approx -20 \text{ K km}^{-1}$$

$$\text{Earth's Troposphere} \approx -7 \text{ K km}^{-1}$$



# CONVECTIVE TRANSPORT

Convective energy transport is a **turbulent** process by which hotter, deeper parcels of fluid rise, forcing cooler fluid to sink, and **carrying energy upward**.

If you watch a pot of water on the stove, convection does not begin the moment the heat is applied to the bottom.

Instead, a temperature gradient between the heating element and the surface must build.

Convection begins only when it reaches a **critical value**.

This critical gradient is called the **adiabatic temperature gradient**.





# CONVECTIVE STABILITY

Consider a small blob of fluid, in a star or a cooking pot.

It has pressure  $P_b$  and density  $\rho_b$ , compared to the ambient pressure  $P$  and density  $\rho$ .

If the blob is perturbed upward, to a lower pressure region,  $P + dP$  ( $dP < 0$ ), it will **expand** until  $P_b + dP_b = P + dP$ .

What happens next depends on the density. If it is denser than the new surroundings ( $\rho_b + d\rho_b > \rho + d\rho$ ), it will **sink** back down and the fluid is stable.

However, if  $\rho_b + d\rho_b < \rho + d\rho$ , the blob is **buoyant** and will keep rising, marking the onset of convection.

Since initially  $\rho_b = \rho$ , the **stability condition** is  $d\rho_b > d\rho$ .



# ADIABATIC EXPANSION

If this blob moves upward rapidly, there is insufficient time for it to **exchange heat** with the ambient medium.

A process in which heat is neither gained or lost is called *adiabatic*. Adiabatic processes are also **isentropic**.

For an adiabatic process  $PV^\gamma$  is **conserved**.

$\gamma$  is the adiabatic index (e.g.,  $\gamma = 5/3$  for monatomic gas).

Writing this in terms of density  $P\rho^{-\gamma}$  and taking the derivative

$$\frac{d\rho_b}{\rho_b} = \frac{1}{\gamma} \frac{dP_b}{P_b}$$

Applying the initial condition,  $\rho_b = \rho$  &  $P_b = P$ , and the requirement of hydrostatic equilibrium  $dP_b = dP$ ,

$$d\rho_b = \frac{\rho_b}{\gamma} \frac{dP_b}{P_b} = \frac{\rho}{\gamma} \frac{dP}{P} = \frac{\rho}{\gamma P} \frac{dP}{dr} dr$$



# STABILITY CONDITION

Applying this expression for  $d\rho_b$  to the **stability condition**

$$d\rho_b = \frac{\rho}{\gamma P} \frac{dP}{dr} dr > d\rho = \frac{d\rho}{dr} dr$$

Simplifying yields  $\frac{1}{\gamma P} \frac{dP}{dr} > \frac{1}{\rho} \frac{d\rho}{dr}$

To compare the **convective stability** to the **radiative energy transport** requires conversion to  $dT/dr$ . For an **ideal gas**,

$$\frac{dP}{dr} = \frac{\rho k}{\mu m_p} \frac{dT}{dr} + \frac{kT}{\mu m_p} \frac{d\rho}{dr} = \frac{P}{T} \frac{dT}{dr} + \frac{P}{\rho} \frac{d\rho}{dr}$$

Rearrangement reveals,  $\frac{1}{\rho} \frac{d\rho}{dr} = \frac{1}{P} \frac{dP}{dr} - \frac{1}{T} \frac{dT}{dr}$

Thus the stability condition can be written,  $\frac{1}{\gamma P} \frac{dP}{dr} > \frac{1}{P} \frac{dP}{dr} - \frac{1}{T} \frac{dT}{dr}$



# ADIABATIC GRADIENT

Grouping the  $dP/dr$  terms, and multiplying by  $T$  yields

$$-\left(1 - \frac{1}{\gamma}\right) \frac{T}{P} \frac{dP}{dr} > -\frac{dT}{dr}$$

The left-hand side of this equation is called the *adiabatic temperature gradient*. At any point that the actual temperature gradient (the right-hand side) obeys this relation, **convection is suppressed** and radiative transport dominates.

Where this relation is not met, convection results, **forcing** the actual temperature gradient toward the adiabatic temperature gradient.

The **equation of convective energy transport** is therefore

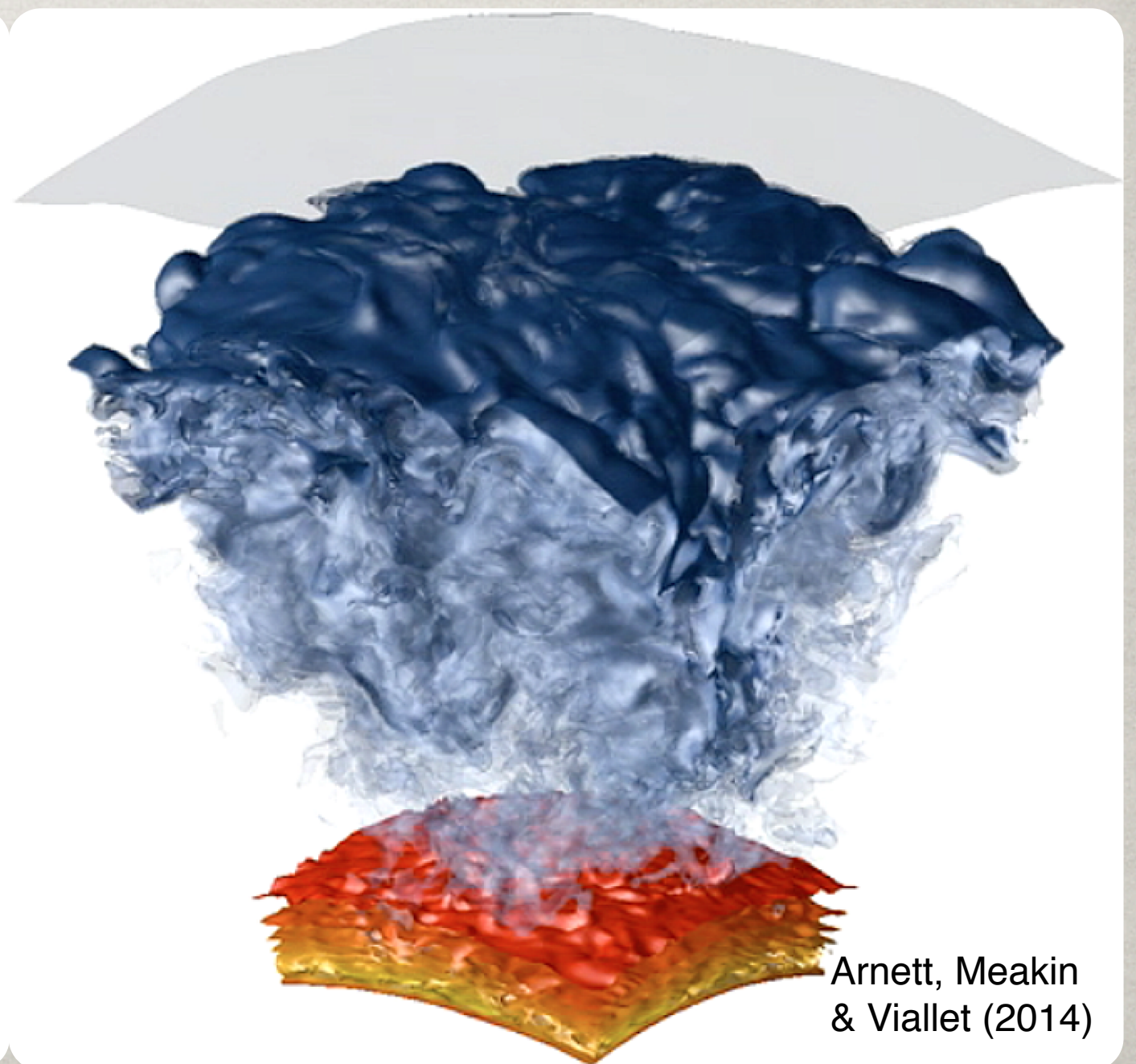
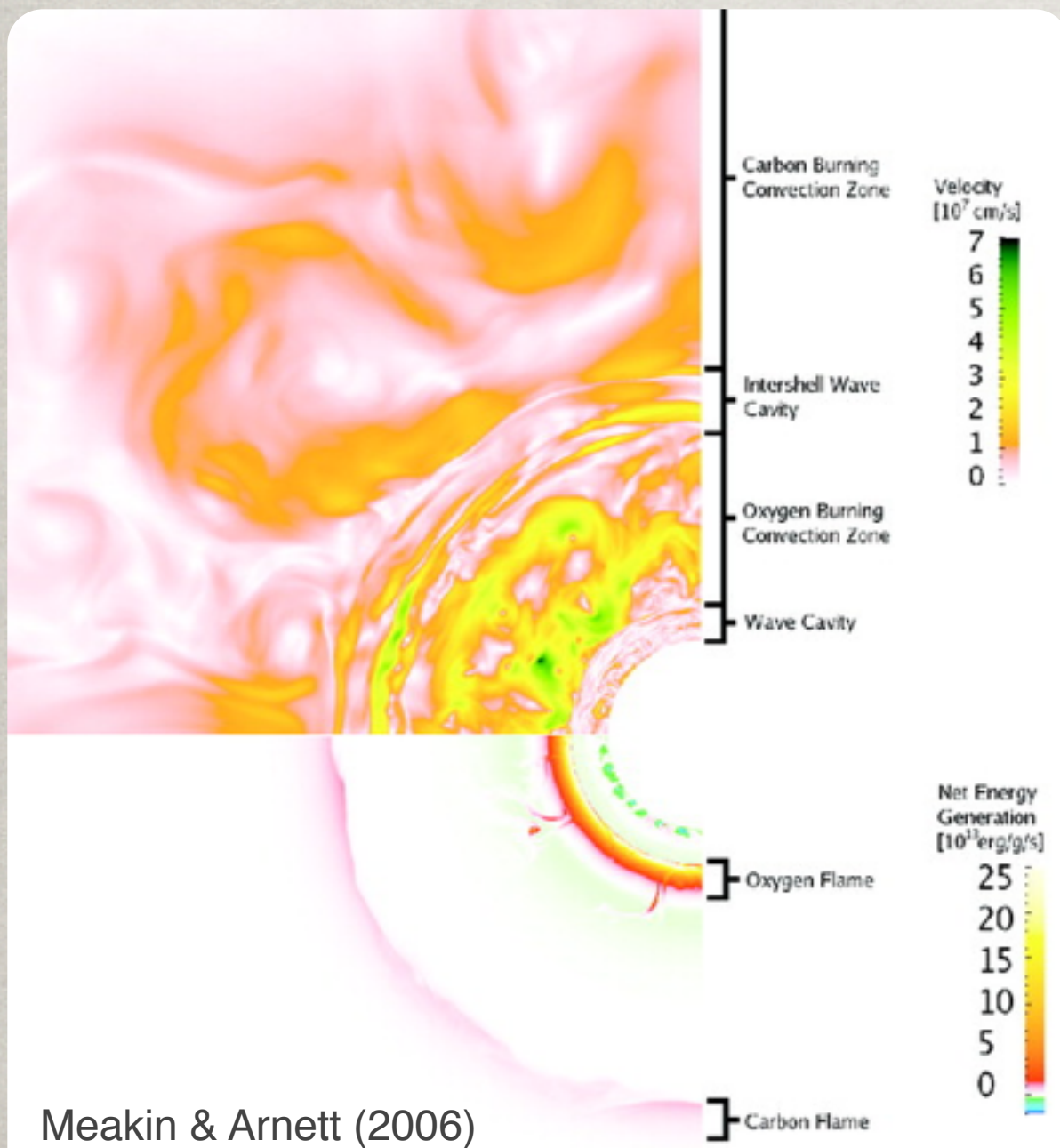
$$\frac{dT}{dr} = \left(1 - \frac{1}{\gamma}\right) \frac{T(r)}{P(r)} \frac{dP}{dr}$$



# STELLAR CONVECTION

Convection is very important in [stellar evolution](#).

Its proper treatment is a topic of much [research](#) (& [debate](#)).





# RAYLEIGH-TAYLOR

Another instability of interest to nuclear astrophysics is the **Rayleigh-Taylor instability**.

When a denser fluid lies “over” a lighter fluid, the amplitude,  $\eta$ , of a perturbation of the interface of wavelength  $2\pi/k$  will **grow exponentially**

$$\eta(t) = \eta_0 \exp[(Agk)^{1/2} t]$$

where  $A$  is the Atwood number  $A \equiv \frac{\rho_u - \rho_l}{\rho_u + \rho_l}$

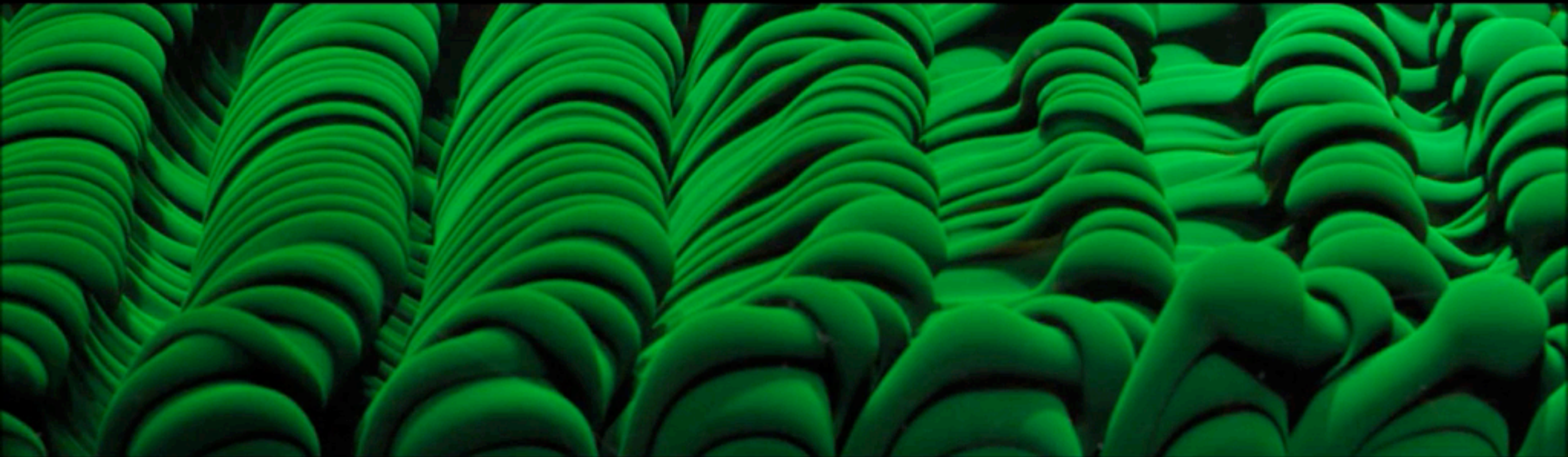
This ideal fluid solution is modified by **viscosity and diffusivity**, which inhibit high-wavenumber (short wavelength) growth.

This also occurs when **acceleration**, as by a shock, takes the place of an effective gravity.



# 3D RT

## Rayleigh-Taylor instability between two stable stratifications



Megan Davies Wykes and Stuart Dalziel

DAMTP, University of Cambridge, UK

[arxiv.org/abs/1210.2591](https://arxiv.org/abs/1210.2591)

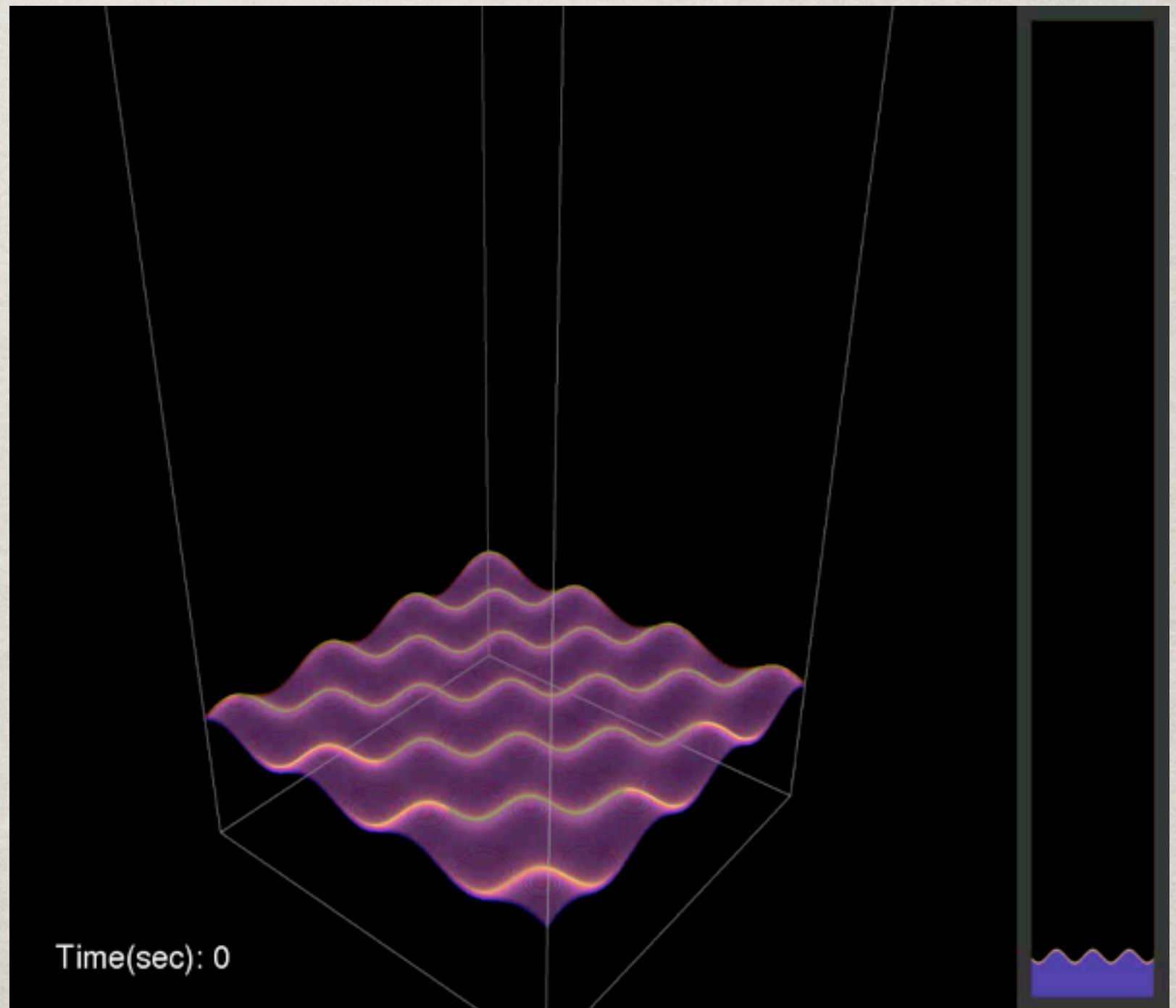


# THERMONUCLEAR RT

With **ongoing energy production** from nuclear reactions, the hot, low density matter remains lower in density as it rises.

This allows **successive generations** of Rayleigh-Taylor instability to build on each other.

Here we see a narrow region from a **thermonuclear supernovae**.





# KELVIN-HELMHOLTZ

Another commonly encountered hydrodynamic instability is the **Kelvin-Helmholtz** instability.

It occurs when a **velocity shear** exists between two layers in a fluid.

The motion of the higher velocity fluid introduces **vorticity** at the interface.

The unstable interface can **grow** to include the entire volume.





# KELVIN-HELMHOLTZ IN 3D

In 3D, KH starts as in 2D, but soon develops **lateral motions**.



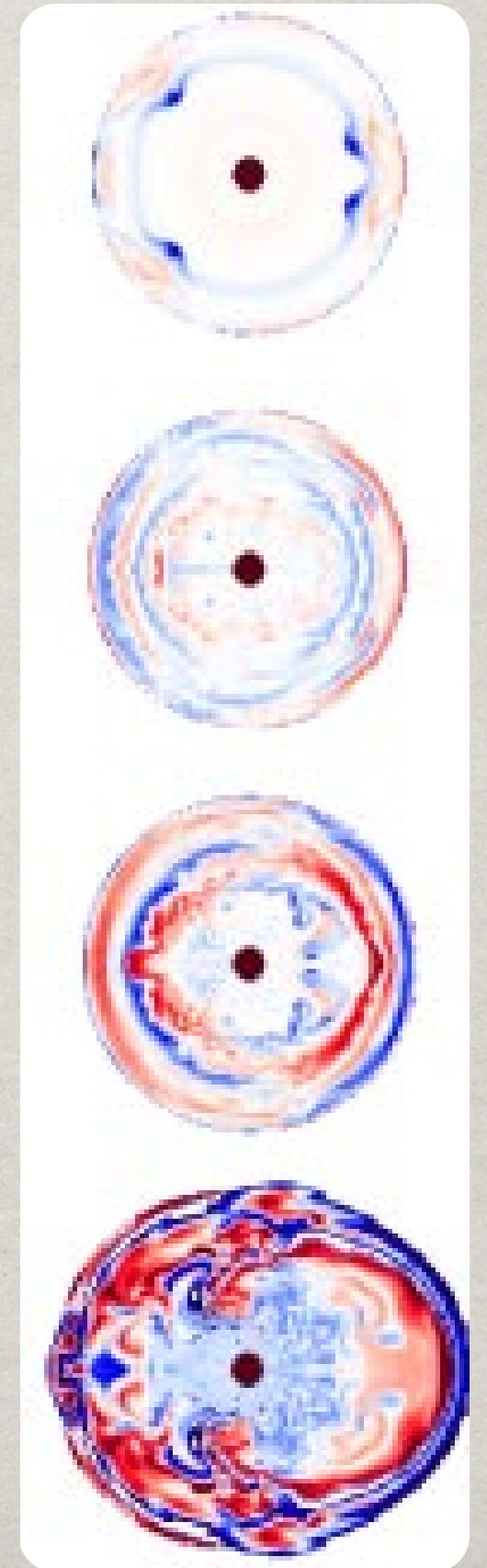


# STANDING ACCRETION SHOCK

Numerical simulations of a **standing accretion shock**, a phenomenon thought to occur during core-collapse supernovae, led to the discovery of a new instability by Blondin & Mezzacappa (2003).

Studied by many groups using **simplified hydrodynamic models** and seen by most groups doing **realistic supernova models**, in cases where the shock stalls for a sufficient time.

However, the mechanism is still a **subject of debate**, with some arguing it is an acoustic instability and others arguing advective-acoustic.

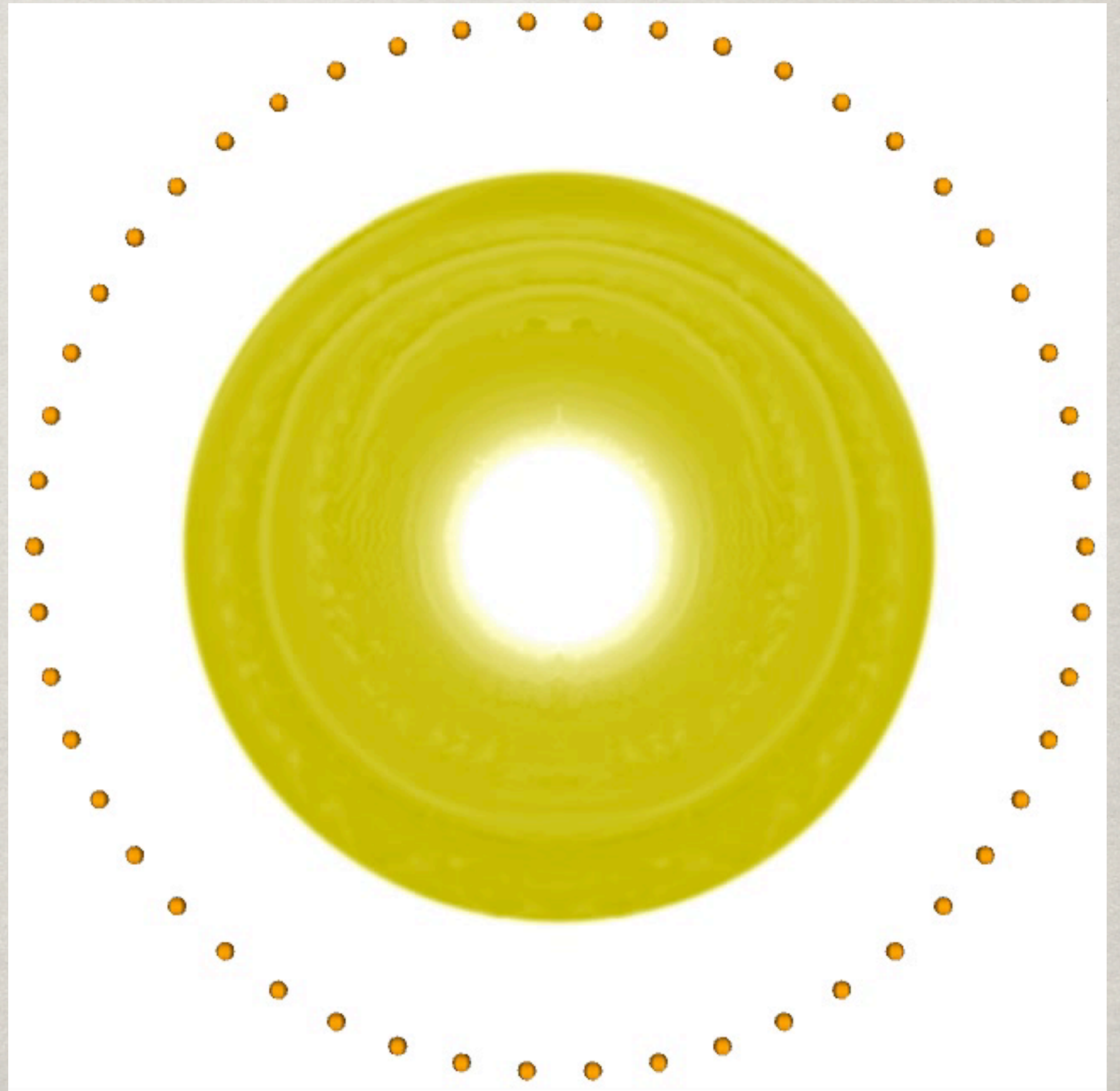




# SASI IN 2D

In 2D, the SASI is dominated by a **sloshing mode** dominated by the  $l = 1$  component.

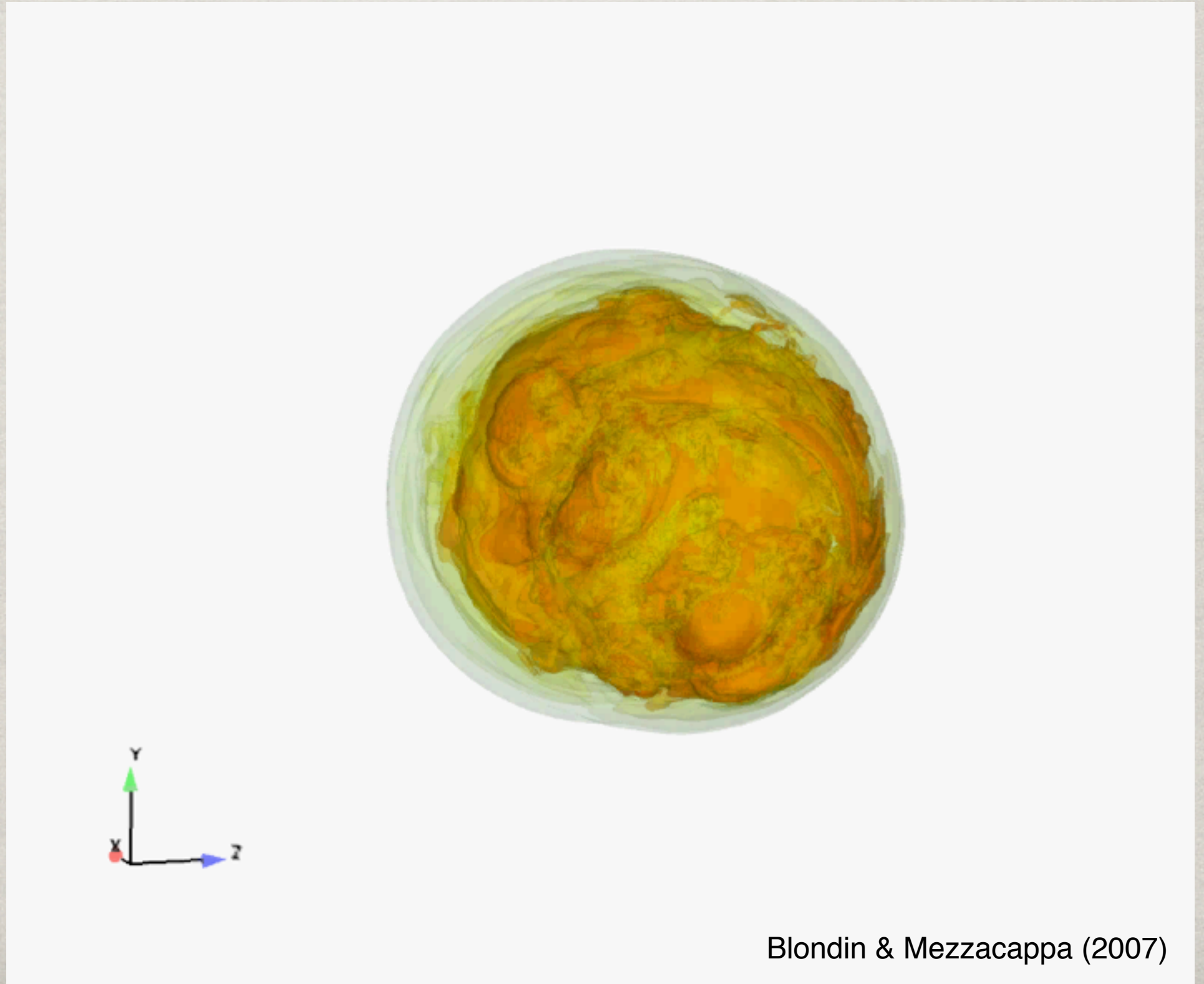
The net effect is to **push the accretion shock boundary** outward.





# SASI IN 3D

In 3D, the  $l = 1$  sloshing mode transforms to an  $m = 1$  spiral mode.

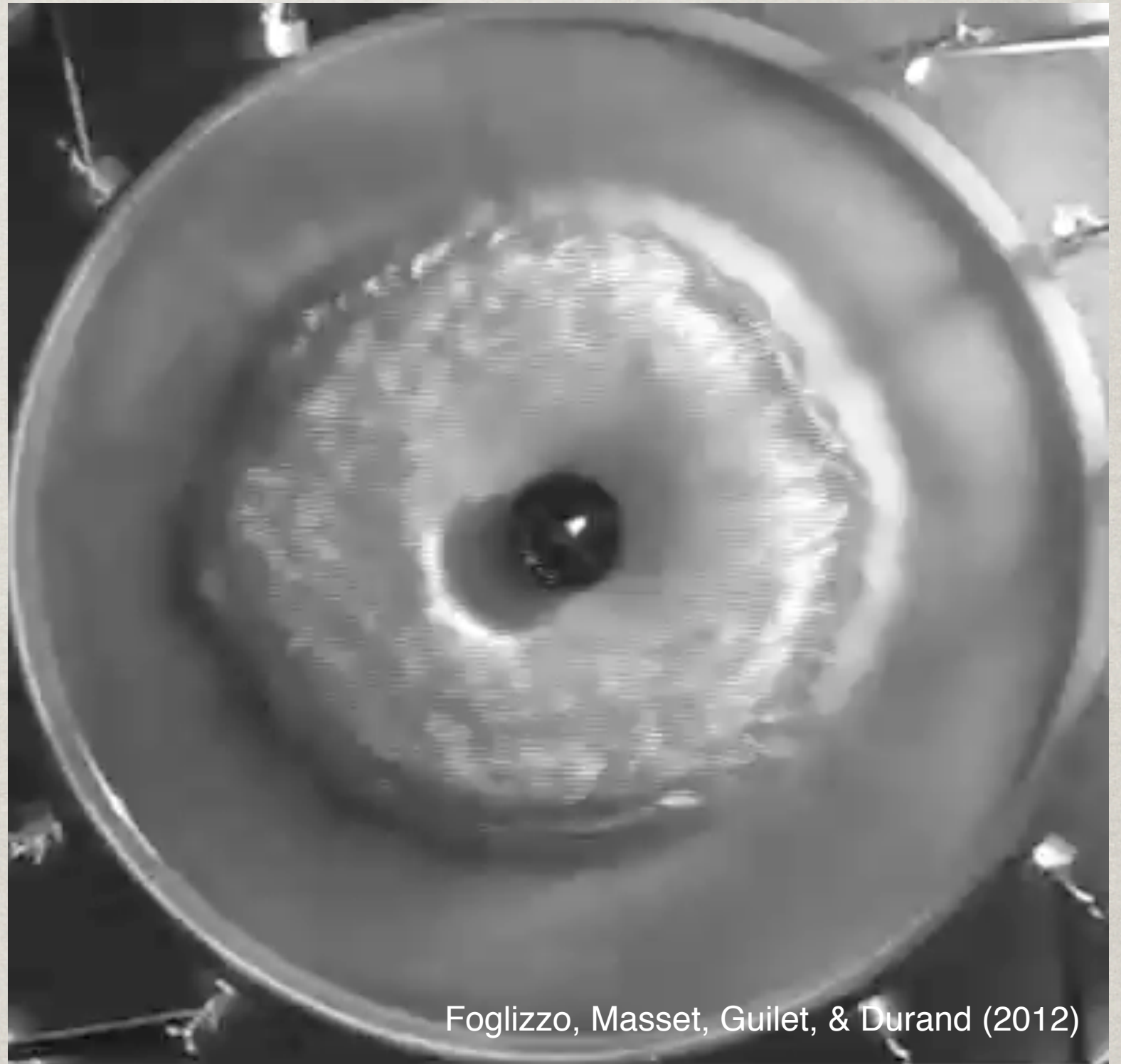




# SHALLOW WATER SUPERNOVA?

Recently, Foglizzo and collaborators discovered a similar instability in a **shallow water** system, SWASI, a Shallow Water Analogue of a Shock Instability.

These also show initial **sloshing modes** that sometimes transition to **spiral modes**.



Foglizzo, Masset, Guilet, & Durand (2012)



# CONCLUSIONS

Equations of Hydrodynamics are **conservation equations** for mass, momentum and total energy, as modified by external surface and body forces, internal energy generation and surface energy flow.

The **Equation of State** closes the system of equations.

Godunov methods, including PPM, use the solution of **Riemann problems** to calculate fluxes across cell boundaries, allowing better capture of shocks and other sharp features.

**Convection and a number of other instabilities** (Rayleigh-Taylor, Kelvin-Helmholtz, SASI) are important for nuclear astrophysics by altering the fluid flow in which nuclear reactions occur and the distribution of the newly formed elements.